

Roger Stanley supporting information

Documents submitted:

- **NIA Assessment for Committee** — a concise (1 page/2 sides) summary of my objection together with a summary of my review of the NIA.
- **Appendix 1 — Critique of the Noise Impact Assessment** — my detailed review of the NIA, submitted previously to the planning authority
- **Noise Impact Assessment (NIA)** — the applicant's own submitted report (August 2024), included for your and the Committee's ease of reference
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By way of brief justification for submitting this package: the NIA was submitted by the applicant as their primary evidence on noise impact. My critique demonstrates that even on the applicant's own figures and methodology — specifically the +8 dB difference under night-time conditions classified on their own scale as "Adverse Impact Likely" under BS4142 — the assessment indicates adverse impact rather than supporting the application. This goes directly to the prevention of public nuisance licensing objective and I believe it is important that the panel has sight of both the NIA and the critique in order to assess the applicant's evidence properly.

I would be grateful if these documents could be included in the committee bundle and distributed to all parties accordingly.

Please also find my completed hearing notice form below.

Kind regards

Roger

60775 – NIA ASSESSMENT FOR COMMITTEE

Bobby's, 21 & 25–26 The Parade, Shrewsbury, SY1 1DL | Ref: 60775 |
Written Addendum submitted by Roger Stanley, Flat B5, The Court, SY1 1DY

1. WHO I AM AND WHY I AM WRITING

I am Roger Stanley and I live directly above the terrace, which is the subject of this application. I have already submitted a formal objection on the grounds of **prevention of public nuisance** (ref: 60775, dated 30th March 2026). I am submitting this additional summary to highlight that the applicant's own Noise Impact Assessment does not support their case — and to ensure this analysis is available to the committee. This application asks the Sub-Committee to allow the terrace to be used until 8.30pm — something that has already been refused, or accepted by the applicant as a condition, **four times** by the relevant authorities on exactly these grounds.

2. A CLEAR AND CONSISTENT TRACK RECORD OF REFUSAL

This is not a new issue. Evening use of this terrace has been considered and rejected at every turn:

- **July 2024** – Licensing Sub-Committee refused terrace use beyond 17:00, finding it would cause unacceptable harm to residential amenity.
- **June 2025** – Planning permission refused on identical grounds (ref: 25/01540/VAR).
- **February 2026** – New planning permission granted for a covered terrace structure, but only on condition that it closes at 17:00 — a condition the applicant expressly accepted (ref: 25/04731/FUL).
- **April 2026** – Planning application to vary those hours refused again (ref: 26/00847/VAR), with the Council's Environmental Protection officer confirming the position remains unchanged.

This application seeks to go further still — to 20:30 — more intensive than even the previously refused schemes. **Nothing material has changed.**

3. THE CHARACTER OF THIS LOCATION

This is not a town centre night-time economy location. The rear of The Parade is quiet and residential in character from 17:00 onwards. All commercial activity ceases. The Council's own Environmental Protection officer described it as having "*a quiet residential tranquillity*" in the evening, with the soundscape reduced to distant traffic and birdsong. Indeed, Bobby's own website describes the location as "*a secret location*" — which is entirely consistent with the character of the area, and directly contradicts any suggestion that this is a busy, noisy environment where evening activity is normal or expected. Introducing an outdoor dining and drinking area with up to 65 covers into this environment would be intrusive and harmful.

4. THE NOISE IMPACT ASSESSMENT DOES NOT STACK UP

The applicant's Noise Impact Assessment (NIA) is the same report submitted in August 2024. It has not been updated. Its conclusions are unreliable for these key reasons:

- **Wrong time of day:** Survey measurements were taken at lunchtime (1–3pm on a weekday), not during the evening periods the application covers. Evening conditions are materially different — lower background noise, louder voices, higher activity.
- **Wrong number of people:** The NIA assumes the terrace holds around 30 people. The actual capacity is approximately 65 covers — more than double. A larger crowd generates significantly more noise.
- **Unrealistic behaviour assumed:** The NIA describes the terrace as a "quiet escape." An outdoor bar-style terrace in the evening — with alcohol — is not a quiet escape.
- **Outdoor kitchen ignored:** The revised structure includes an outdoor kitchen, added under the February 2026 permission. The NIA contains no assessment of kitchen noise or smells.
- **Enclosure may make things worse:** The applicant suggests the new enclosed layout will reduce noise. But for residents directly above, an enclosure can channel and concentrate noise upwards rather than disperse it.

Critically, the NIA's own findings show a +8 dB difference under night-time conditions — which its own scale classifies as "Adverse Impact Likely" under BS4142. Separately, the applicant's own patron noise calculation predicts sound levels at residential windows of just 43.9 dB — only 1 dB below the WHO guideline threshold for sleep disturbance with windows open. That 1 dB margin is based on a terrace of 30 people on a Thursday lunchtime. The actual terrace holds 65 covers on a Friday or Saturday evening. The applicant's own evidence, properly applied, supports refusal.

5. CONCLUSION AND REQUEST

The case against this application is straightforward. Four previous decisions or accepted conditions have established that evening terrace use at this location is unacceptable. The applicant has provided no new or reliable evidence to justify a different outcome. The Noise Impact Assessment is outdated, based on the wrong conditions, and — even on its own flawed terms — indicates adverse impact.

I ask the Sub-Committee to **refuse this application** and uphold the 17:00 limit, consistent with its previous decisions and the planning condition the applicant accepted just two months ago and which planning refused to vary as recently as 14 April 2026.

Appendix 1 – Review of Noise Impact Assessment

This appendix provides a review of the Noise Impact Assessment (NIA) submitted in support of the application.

1. Use of Unchanged Assessment

The NIA appears to be unchanged from the version prepared in August 2024 and therefore does not represent new or materially updated evidence. It does not address the concerns that led to previous refusals.

2. Non-Representative Survey Conditions

Measurements of comparable venues were undertaken during midweek lunchtime periods (approximately 13:00–15:00).

These conditions are not representative of the proposed use, which relates to evening operation (up to 20:30). Evening conditions (especially Friday and Saturday) are materially different due to:

- increased activity levels
- alcohol consumption
- louder and more variable voice levels
- lower background noise

3. Underestimation of Occupancy and Activity

The NIA refers to an outdoor seating area that can “comfortably hold approximately 30 people”.

However, the actual capacity of the terrace is understood to be significantly higher (approximately 65 covers, source: Bobbys). This represents a substantial difference in potential usage.

An assessment based on materially lower occupancy is likely to underestimate noise generation, particularly during peak periods when the terrace would be fully occupied.

An increase in the number of patrons will inevitably increase overall noise levels, and the difference between the assumed and actual capacity is therefore likely to be material.

In addition, the NIA assumes that noise will arise primarily from talking, and describes the terrace as a “quiet escape”.

This does not reflect typical behaviour associated with outdoor dining and drinking environments, where noise can include raised voices, laughter, movement of furniture, and general activity associated with groups of patrons.

Furthermore, the design of the temporary structure was amended under 25/04731/FUL (of which the residents of the Court were not directly informed) and now includes an outdoor kitchen. The additional noise associated with this outdoor kitchen has not been assessed within the NIA.

Although not directly related to noise, it is noted that no assessment of smells or other potential nuisances arising from the outdoor kitchen has been provided.

4. Findings Indicate Adverse Impact

The NIA's own BS4142 assessment indicates a +8 dB difference under night-time conditions, which is classified as "adverse impact likely".

This demonstrates that, even based on the applicant's own assumptions, the proposed use would result in harmful noise impacts.

Predicted noise levels are close to recognised guideline thresholds, leaving little or no margin for variation in real-world conditions. For the reasons highlighted in this Appendix, the figure of +8 dB is likely to be a significant understatement of real-world conditions.

5. Lack of Assessment at Sensitive Receptors

Noise measurements were not undertaken at the residential façades directly overlooking the terrace, and instead rely on modelling.

Given the proximity and direct overlooking relationship, this introduces uncertainty and reduces confidence in the conclusions.

6. Limited Consideration of Internal Residential Conditions

The assessment also does not consider internal noise impacts within the residential properties above, despite their close proximity and direct overlooking relationship, and the likelihood that windows will be open during warmer months.

7. Enclosure Does Not Demonstrate Mitigation

The noise report itself recognises that noise is more intrusive when the source is visible and recommends the installation of a privacy screen. The applicant relies on a revised, more enclosed arrangement as a form of mitigation.

However, given the site layout, with residential properties directly above the terrace, a more enclosed ground-floor configuration may concentrate or channel noise upward rather than reduce it. The submitted material does not demonstrate that this revised arrangement would improve conditions for the residents most affected.

Nothing has been done to address the visible aspect highlighted in the report.

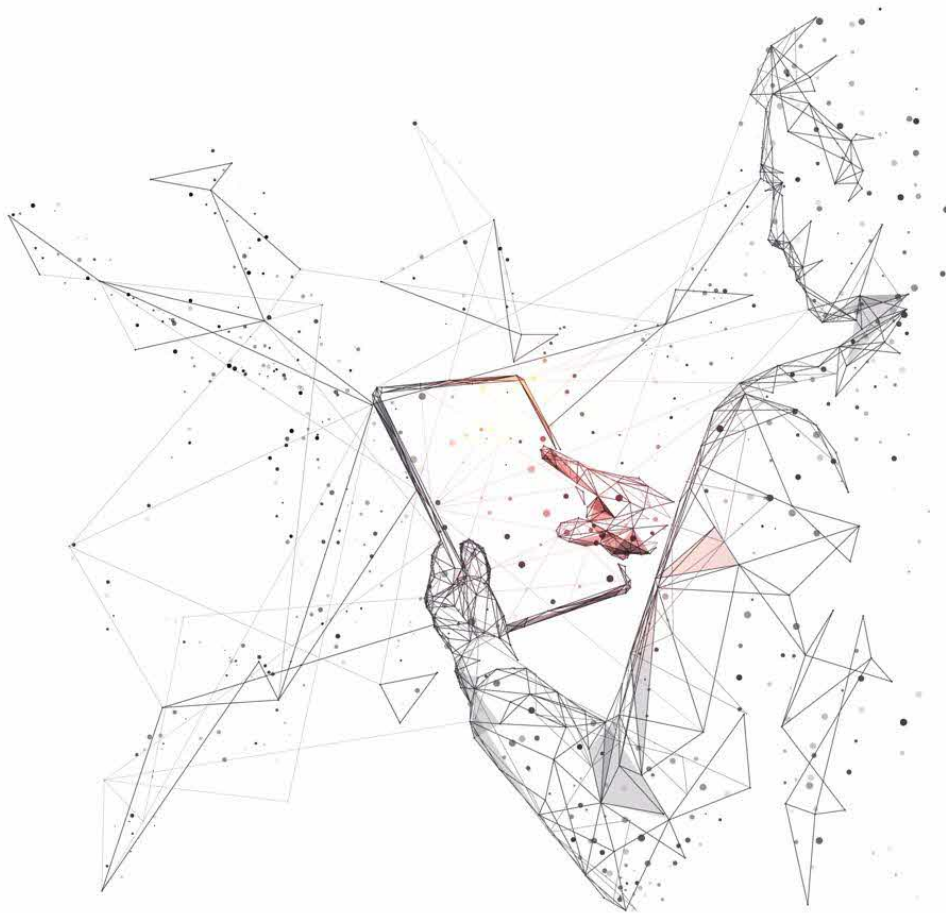
8. Overall Conclusion

The Noise Impact Assessment:

- is based on non-representative survey conditions
- relies on simplified assumptions regarding occupancy and behaviour
- does not consider internal residential conditions
- and indicates adverse impact even on its own terms

Rather than provide a reliable or robust basis for concluding that the proposed extension of terrace hours would be acceptable, the weaknesses, errors and omissions demonstrate a far higher likelihood of adverse impact than previously reported.

AUGUST 12, 2024



BS4142:2014 & OUTDOOR
RESTAURANT/CAFE ASSESSMENT OF
UNITS 25 & 26, THE PARADE, ST
MARY'S PLACE, SHREWSBURY

JAMES FLITTON

E2 HOUSE,
41 Business Park,
S Park Way,
Wakefield
WF2 0XJ

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1.0 Introduction

- 1.0.1 This report has been commissioned to determine the noise impact of the opening Bobbys café/restaurant and outdoor seating area at Units 25 & 26, The Parade, St Mary's Place, Shrewsbury.
- 1.0.2 The assessment has been conducted in line with the BS4142:2014 as the most appropriate assessment methodology. Considerations will also be made to the IOA Good Practice Guide on the Control of Noise from Pubs and Clubs 2003 due to the possibility of outdoor leisure noise.

2.0 Site Details

- 2.0.1 The site is located just off of St Mary's court, to the rear of the Parade shopping area. The restaurant is at ground-floor level with an outdoor seating area proposed in the direction of the River Severn.
- 2.0.2 The area has one other similar café/restaurant a few metres from the proposed area. The first-floor of the Parade, just above the proposed site, has a hairdressers with other commercial-use properties along the first-floor level. The top floors are residential.
- 2.0.3 The closest Noise Sensitive Receptors (NSRs) are located above the hairdressers shop on the 2nd floor of The Parade.
- 2.0.5 The assessment took into account the current ambient and background noise levels in the proposed outdoor area. It was not possible to take a measurement directly in the Parade due to the currently occupying residential and hairdresser units above the proposed development. Measurements were also conducted the outside seating area for the equivalent restaurant/café in the same area as well as another internal measurement at an alternative site owned by the same person as Bobbys.

2.1 Location of Monitors

- 2.1.1 The noise location was chosen based on the available locations as detailed in 2.0.5. This consisted of a 24hr survey at the proposed outdoor seating area and then attended surveys at the existing café/restaurant locations. Images of these locations are shown in figures 1-3 below.

Figure 1 – Outdoor seating area



Figure 2 – Adjacent Café/Restaurant



Figure 3 – Equivalent Café/Restaurant

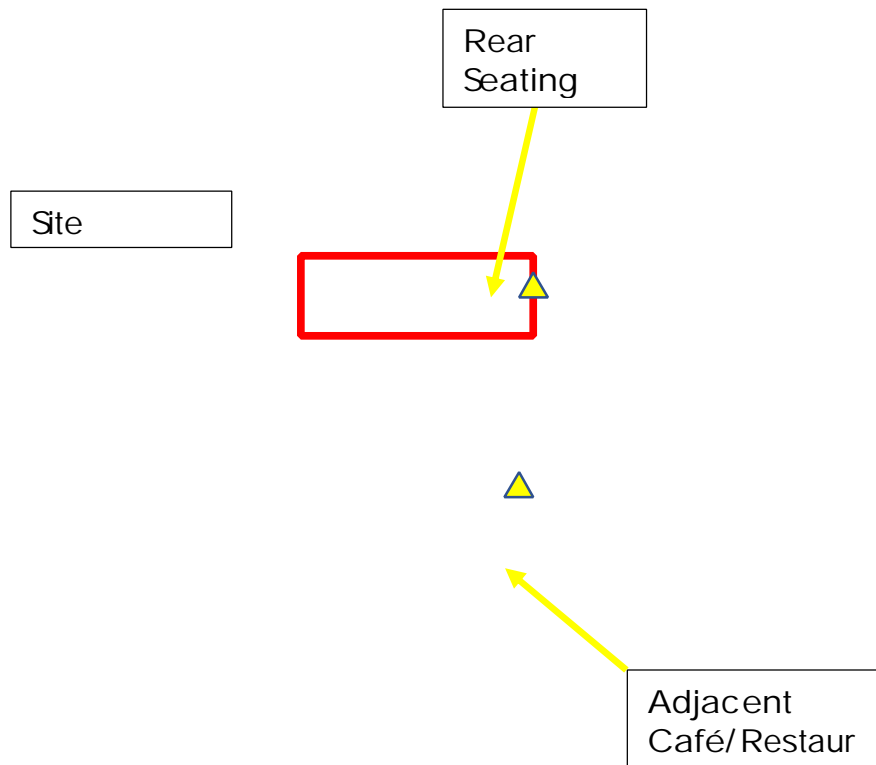


- 2.1.2 Measurements were made in 15 minute periods, on 1 second averaging, to allow for the removal of anomalies and increased accuracy. The data was averaged into L_{Aeq1hr} daytime and $L_{Aeq15min}$ night-time with data also recorded for L_{A90} in both day and night periods for the BS4142:2014 assessment.
- 2.1.3 The monitoring was conducted using 2 x Type 1 NTi XL2 sound level meters with batteries and outdoor microphone protection.
- 2.1.4 All measurements were taken after a field calibration was undertaken to ensure accuracy and repeatability of measurements. Drift was also checked at the end of the measurements for validation purposes.

- 2.1.5 Further data such as wind speed, wind direction, rainfall intensity, temperature and cloud cover were all recorded at the beginning and end of the assessment at the monitoring location.
- 2.1.6 Any anomalies (such as noise by the engineer during setup and collection of the kit) were removed from the survey for a true reflection of the ambient levels in the vicinity. This was done by recording audio throughout the survey at each location and listening back through the files during the analysis process to confirm what was recorded manually during the survey.

2.2 Plan Views of Site with Designated Work Areas

Figure 4



= Monitoring Position for Noise Assessment

3.0 Legislation

3.0.1 The National Planning Policy Framework (NPPF) sets out the Government's economic, environmental and social planning policies for England and "these policies articulate the Government's vision of sustainable development." In respect of noise, Paragraph 174 of the NPPF states the following:

"Planning policies and decisions should contribute to and enhance the natural and local environment by:

e) preventing new and existing development from contributing to, being put unacceptable risk from, or being adversely affected by, unacceptable levels soil, air, water or noise pollution..."

Paragraph 185 goes on to mention:

"Planning policies and decisions should also ensure that new development is appropriate for its location taking into account the likely effects (including cumulative effects) of pollution on health, living conditions and the natural environment, as well as the potential sensitivity of the site or the wider area to impacts that could arise from the development. In doing so they should:

- a) mitigate and reduce to a minimum potential adverse impacts resulting from noise from new development – and avoid noise giving rise to significant adverse impacts on health and the quality of life;
- b) identify and protect tranquil areas which have remained relatively undisturbed by noise and are prized for their recreational and amenity value for this reason;"

3.0.2 The NPPF reinforces the March 2010 DEFRA publication, "Noise Policy Statement for England" (NPSE), which states three policy aims, as follows:

"Through the effective management and control of environmental, neighbour and neighbourhood noise within the context of Government policy on sustainable development:

avoid significant adverse impacts on health and quality of life;
mitigate and minimise adverse impacts on health and quality of life;
and where possible, contribute to the improvement of health and quality of life."

3.0.3 Together, the first two aims require that no significant adverse impact should occur and that, where a noise level which falls between a level which represents the lowest observable adverse effect and a level which represents a significant observed adverse effect, then according to the explanatory notes in the statement:

“... all reasonable steps should be taken to mitigate and minimise adverse effects on health and quality of life whilst also taking into consideration the guiding principles of sustainable development. This does not mean that such effects cannot occur.”

3.0.4. It is possible to apply objective standards to the assessment of noise and the effect produced by the introduction of a certain noise source may be determined by several methods, as follows:

The effect may be determined by reference to guideline noise values. British Standard (BS) 8233:2014 and World Health Organisation (WHO) “Guidelines for Community Noise” contain such guidelines.

Another method is to compare the resultant noise level against the background noise level (L_{A90}) of the area. This is the method employed by BS 4142:2014 to determine the likelihood of complaint from noise of an industrial nature. It is best suited to the assessment of steady or pseudo-steady noise.

3.0.5 British Standard 8233:2014 is principally intended to assist in the design of new dwellings; however, the Standard does state that it may be used in the assessment of noise from new sources being brought to existing dwellings.

3.0.6 The WHO guideline values are appropriate to what are termed “critical health effects”. This means that the limits are at the lowest noise level that would result in any psychological or physiological effect.

The WHO Community Noise guideline noise values are summarised in the following table:

Table 1

Guidance Document	L_{AeqT}	L_{AMax}	Outcome
World Health Organisation “Community Noise 2000”	55dB		Serious annoyance, daytime and evening. (Continuous noise, outdoor living areas)
	50dB		Moderate annoyance, daytime and evening. (Continuous noise outdoor living areas).
	35dB		Moderate annoyance, daytime and evening. (Continuous noise dwellings, indoors)
	30dB		Sleep disturbance, night-time (indoors)
	45dB		Sleep disturbance at night, windows open (Outside Bedroom:

		60dB	Sleep disturbance, windows open at night. (Noise peaks outside bedrooms, external level).
		45dB	Sleep disturbance at night (Noise peaks inside bedrooms, internal level)

3.1 BS4142:2014 +A1 (2019)

- 3.1.1 Noise effects on residential properties have been assessed according to the guidance in BS 4142:2014. This standard primarily provides a numerical method by which to determine the significance of sound of an industrial nature (i.e. the 'specific sound' from the proposed development) at residential sensitive receptors.
- 3.1.2 The specific sound level may then be corrected for the character of the sound (e.g. perceptibility of tones and/or impulses), if appropriate, and it is then termed the 'rating level', whether or not a rating penalty is applied. The 'residual sound' is defined as the ambient sound remaining at the assessment location when the specific sound source is suppressed to such a degree that it does not contribute to the ambient sound.
- 3.1.3 According to BS 4142:2014, the background sound levels adopted for the assessment should be representative of the periods being assessed. The standard recommends that the background sound level should be collected from continuous measurements of normally not less than 15-minute intervals. However, the Standard states that there is no 'single' background sound level that can be derived from such measurements. It is particularly difficult to determine what is 'representative' of the night-time period because it can be subject to a wide variation in background sound levels between the shoulder night periods.
- 3.1.4 The method chosen for this section of the report is to use the data collected at the nearest NSR for the day and night periods to provide the ambient and background noise levels. The mode $L_{Aeq_1hr(Day)}$ and $L_{Aeq_15min(Night)}$ value will then be used for each time period over the course of the measurement as the most appropriate way of creating a representative value.
- 3.1.5 The specific sound levels have been determined separately in terms of the L_{Aeq_1hr} during the daytime L_{Aeq_15min} during the night-time. Daytime is typically between 07:00 and 23:00 hours and night-time is typically between 23:00 and 07:00 hours, so these periods have been adopted for this assessment.
- 3.1.6 At each of the most likely sensitive receptor locations, the rating level has been determined from the predicted specific sound level. Where it has considered it to be appropriate, a rating penalty has been applied for tonality, impulsivity and/or intermittent specific sounds as described in the commentary to

paragraph 9.2 of BS4142:2014. This has been applied with consideration for the main sound sources from site that contribute to the level of specific sound at the receptor location.

- 3.1.7 As per the requirements of the standard, an initial estimate of the impact of the specific sound has been obtained by subtracting the measured background sound level from the rating level of the specific sound. Table 3 provides the initial evaluation of impact following this method.

Table 3

Magnitude	Difference Between rating Level and Background Level	Comments
High	+10dB	Significant Adverse impact Likely
Medium	+5 to +10dB	Adverse impact Likely
Low	0 to +5 dB	Adverse impact unlikely
Negligible	Less than 0dB	Adverse impact unlikely
No Change	-10 dB	No adverse impact

- 3.1.8 Following the initial evaluation of impact, the context of the sound has also been considered, which is a key requirement of the Standard. In evaluation of the context, the following factors have been considered:

- the absolute level of the sound;
- the character and level of the residual sound compared to the character and level of the specific sound and
- the sensitivity of the receptor and whether dwellings or other premises used for residential purposes will already incorporate design measures that secure good internal and/or outdoor acoustic conditions.

- 3.1.9 Despite the fact that section 1.3 of BS4142:2014 states that entertainment noise is not an intended use for the standard, it is still one of the best methods of assessing this type of noise due to the options of tonality, impulsive and character penalties that can be applied to influence the rating level.

3.2 IOA Good Practice Guide on the Control of Noise from Pubs and Clubs 2003

- 3.2.1 In the absence of an official standard for the control of noise from Cafes, Restaurants, Pubs and clubs there have been various studies conducted. One of these was published by the IOA in 2003 and gives general guidelines and

advice on measurements, assessment and control of pub noise. Although the proposed development is not a pub or club, it is still seen as one of the closest methodologies that provide additional robustness to a standard BS4142:2014 assessment.

3.3.2 DEFRA also published Phase 1 & 2 reports which form the basis for most current assessments of entertainment noise from pub and clubs with recommendations as to which measure to use for assessments of entertainment noise. This includes specifying that outdoor crowd noise of small gatherings with no music is likely to produce L_{Aeq} values of 65-70dBA.

3.3.3 The IOA Good Practice Guidelines produced a table and assessment methodology to help with assessments of pubs/clubs. This is shown in table 4 below:

Table 4

Event Frequency	Suggested Regulations	Outcome if Criteria Met
Entertainment < 30times/ year	L_{Aeq} , 15mins (EN) should not exceed L_{A90} (WEN) by more than 5dB.	EN will generally be audible but not overly obtrusive inside noise sensitive properties
Entertainment > 30 times/year	L_{Aeq} (EN) should not exceed L_{A90} (WEN) by more than 5dB and the L_{10} (EN) should not exceed L_{90} (WEN) by more than 5dB in any 1/3 octave band between 40 and 160Hz	EN will generally be audible but not overly obtrusive inside noise sensitive properties
Entertainment > once/week or continues beyond 2300hrs	L_{Aeq} (EN) should not exceed L_{90} (WEN) and L_{10} (EN) should not exceed L_{90} (WEN) in any 1/3 octave band between 40 and 160Hz	EN will be virtually inaudible inside noise sensitive properties.

EN = Entertainment noise level

WEN – Representative background noise level without entertainment noise

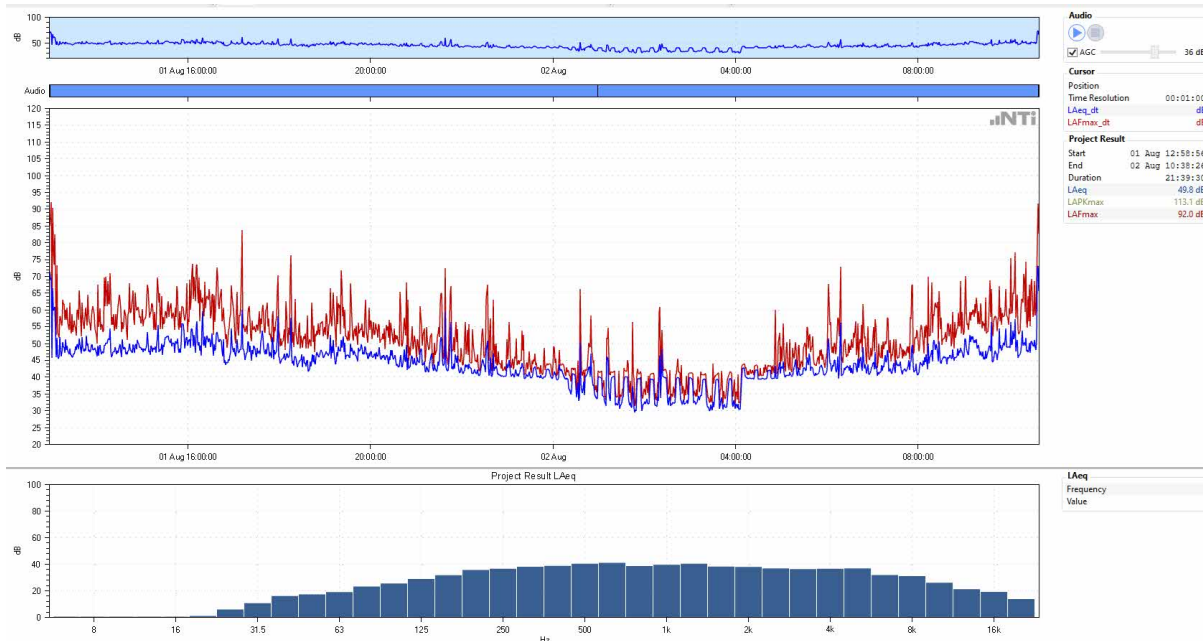
4.0 Results

4.1 – Background/External Monitoring 12.58pm 01/08/24 – 10.38am 02/08/24

Table 5

Time Period	Start Date/Time	L _{Amax}	L _{Aeq1hr} (Mode)	L _{Aeq15min} (Mode)	L _{A90}
Day (0700-2300)		83.6dBA	49.1dBA		43.2dBA
Night (2300-0700)		72.8dBA		39.8dBA	35.3dBA

Figure 4



Comments

Mainly ambient noise from distant traffic. Some on/off generator noise audible through the night period from an adjacent site

*based on Appendix C

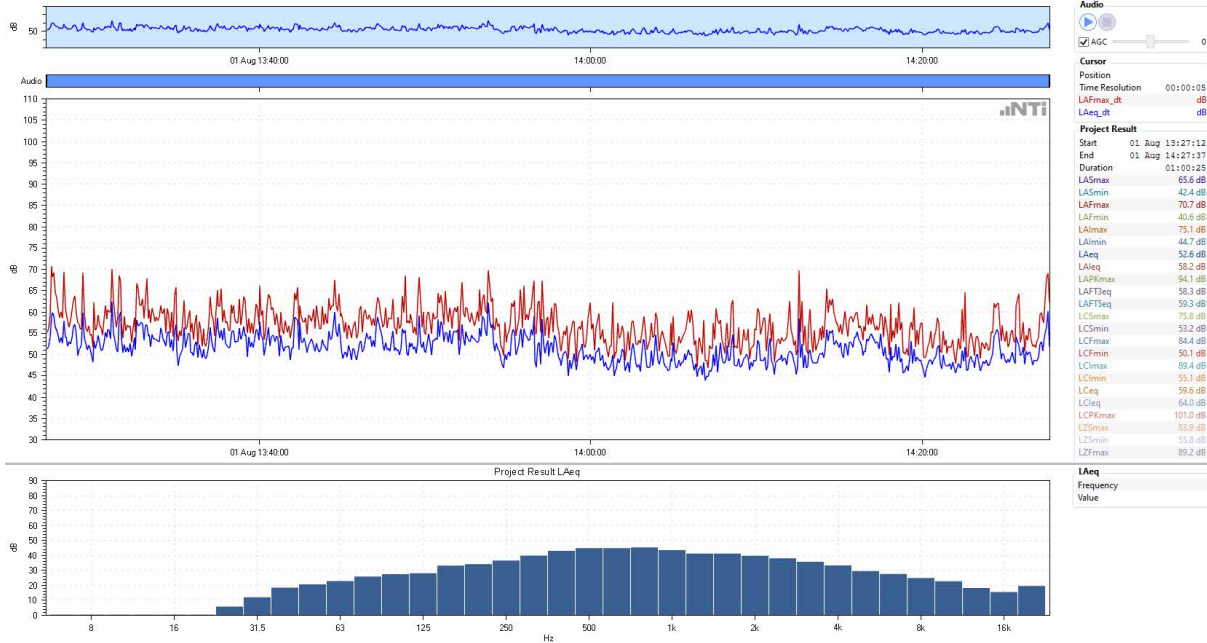
Cloud Cover	Temperature (Celcius)	Presence of fog/snow/ice	Wind Speed (m/s)	Wind Direction
2	18	No	0.4	NE
4	19	No	1.5	ENE

4.2 – External Levels – Adjacent Café/Restaurant 13.27pm 01/08/24 – 14.27pm 01/08/24

Table 6

<i>Time Period</i>	Start Date/Time	L _{Amax}	L _{Aeq1hr} (Mode)	L _{Aeq15min} (Mode)	L _{A90}
<i>Day (0700-2300)</i>		83.6dBA	52.6dBA		46.5dBA

Figure 5



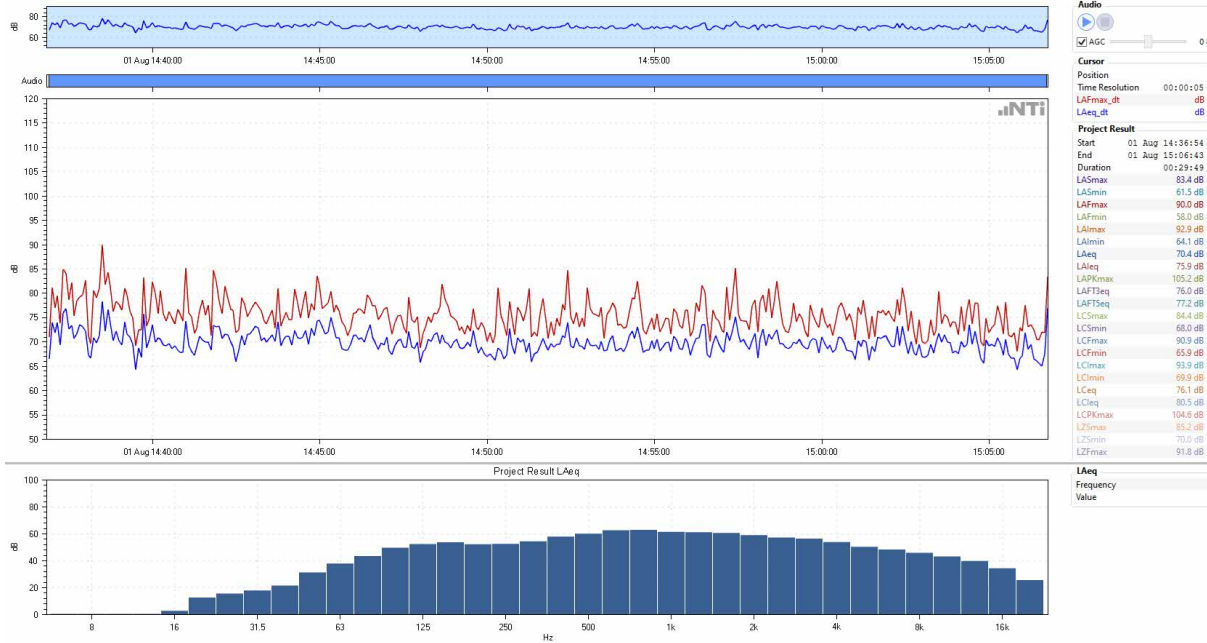
Cloud Cover	Temperature (Celcius)	Presence of fog/ snow/ ice	Wind Speed (m/ s)	Wind Direction
2	18	No	1.1	NE

4.3 – Internal Levels – Equivalent Café/Restaurant (Dough & Oil) 14.36pm 01/08/24 – 15.06pm 01/08/24

Table 7

Time Period	Start Date/Time	L _{Amax}	L _{Aeq1hr} (Mode)	L _{Aeq15min} (Mode)	L _{A90}
Day (0700-2300)		90.0dBA	70.7dBA		65.1dBA

Figure 6

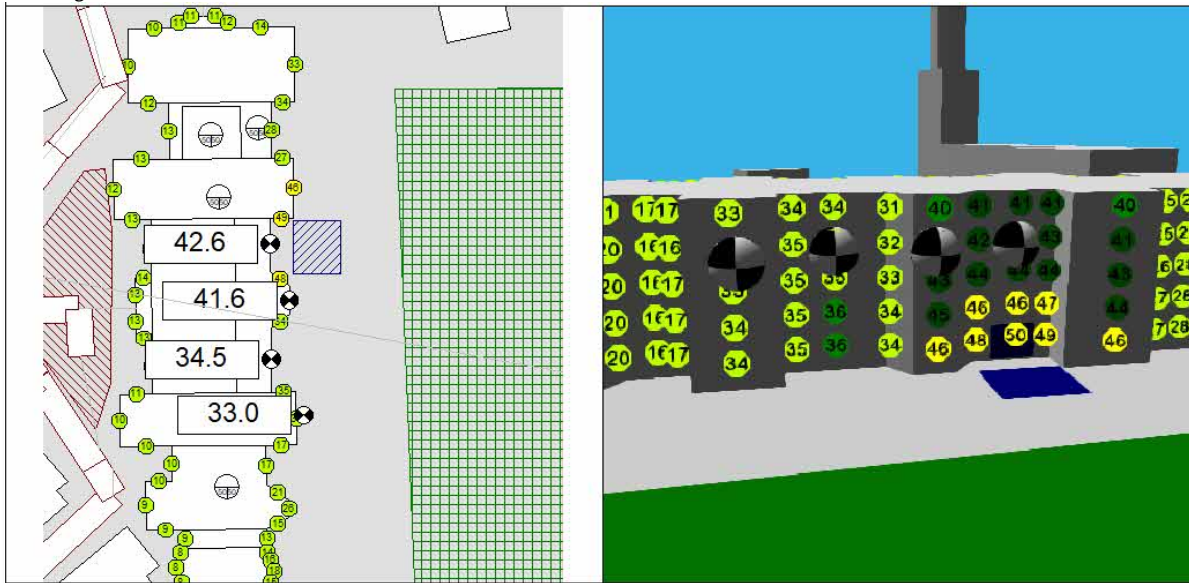


5.0 Analysis of Results

5.1 Data Assessment

- 5.1.1 As the exact NSR (Noise Sensitive Receptor) locations were not available the assessment has been conducted by collecting background data in the area that will be used as the outdoor space for the café/restaurant (4.1), an attended measurement at the similar venue approximately 50m from the proposed (4.2), and finally an internal measurement taken at an equivalent café/restaurant during a busy lunch period to use for break-out noise measurements.
- 5.1.2 The background/ambient/residual noise levels were measured over a period of 24 hours and, despite not being at the façade of the NSR, are considered representative for the soundscape of the area.
- 5.1.3 The similar venue measurement was taken with the outside area full during full service. Although there are possible variations in guests through a 'typical' day/evening, these levels were considered to be representative when the staff at the venue were asked for their experiences. The indoor levels at the equivalent venue called the Dough & Oil. This was also done during a busy lunch service to give a representative noise value for the proposed site.
- 5.1.4 The measured values from the existing outdoor area were 53dBA approx. 3m from the central part of the area, and the representative indoor levels were 71dBA when both values are rounded. A value of 3dB has then been added to each of these figures to cover for more worst-case deviations in the measured values over the averaged time period. These values have then been added into the noise model to produce the predicted noise impact values at the NSF facades and therefore the likely level of adverse impact in accordance with BS4142:2014. As the source is not currently present the ambient, residual and background noise levels have all been taken from the measurement values taken on site, with the specific noise level predicted by the CadnaA noise modelling software.
- 5.1.5 Figure 7 shows the predicted noise impact from the introduction of both the restaurant area and the outdoor seating area. These predictions are on the basis that the restaurant door is left open, which it may not always be, and therefore provides the worst-case scenario for the noise impact from the proposed development. The full calculation output tables for each receiver point are shown in appendix D.

Figure 7



5.1.6 Based on the above calculation the specific noise level for the proposed café/restaurant and outdoor seating area would be 43dBA at the nearest noise sensitive receptor window, and 42dBA, 35dBA and 33dBA at the other nearest residential facades on the higher floors of the Parade. Again, this is with the doors open and the outdoor seating area at the measured levels plus 3dB.

5.1.7 The highest values have then been used in the BS4142:2014 calculation table shown below as table 8.

Table 8

<i>Measurement Type</i>	<i>Parameter</i>	<i>Result</i>	<i>Comment</i>
Day			
<i>Ambient sound</i>	LAeq	49 dBA	Measured at Proposed Outdoor Seating Area
<i>Residual sound level</i>	LAeq1hr	49dBA	Measured at Proposed Outdoor Seating Area
<i>Background sound level</i>	LA901hr	43 dBA	Measured at Proposed Outdoor Seating Area
<i>Specific Sound Level</i>	LAeq1hr	43dBA	Predicted at NSR facade

<i>Acoustic Feature Correction</i>	dBA	+0dBA	No tonality or impulsivity expected
<i>Rating Level</i>	dBA	43 dBA	
<i>Difference of Background vs Rating level</i>	dBA	-0dB	
<i>BS4142:2014 rating</i>			Low Chance of Adverse impact
Night			
<i>Ambient sound</i>	L _{Aeq}	40dBA	Measured at Proposed Outdoor Seating Area
<i>Residual sound level</i>	L _{Aeq15mins}	40dBA	Measured at Proposed Outdoor Seating Area
<i>Background sound level</i>	L _{A9015mins}	35 dBA	Measured at Proposed Outdoor Seating Area
<i>Specific Sound Level</i>	L _{Aeq15mins}	43dBA	Predicted at NSR facade
<i>Acoustic Feature Correction</i>	dBA	+0dBA	No tonality or impulsivity expected
<i>Rating Level</i>	dBA	43 dBA	
<i>Difference of Background vs Rating level</i>	dBA	+8dB	
<i>Likelihood of complain</i>			Adverse impact likely

5.1.7 As the BS4142:2104 is not strictly applicable to pub/club noise the report will also examine the figures against the IOA guidelines for Pubs & Clubs. The extract in Table 4 earlier in this document is for venues that continue beyond 11pm. As the external seating areas is not to be used beyond 9pm, and there is no external music to be played in the area, this aspect of the guidance is not seen as relevant. It does, however, reinforce the decision not to have music playing externally as the venue would move into the category for likelihood of complaints during the day. Table 8 also shows that opening beyond 11pm (again this is not the plan of the proposed restaurant/café) would make adverse impact likely on the residential dwellings in the area.

5.2 Patron Noise

- 5.2.1 The final stage to this assessment is to examine Patron noise. This is looking at the rear outdoor seating area in isolation and any noise that may emanate from this location. The DEFRA report on pubs and bars stated that small crowds in a venue would be assumed to have a L_{Aeq} value of 65-70dB. This figure is consistent with the levels measured during this assessment both externally and internally. The Dough & Oil produced an internal level of 71dBA whereas the adjacent café/restaurant measured approximately 68dB in the central point of the outdoor area. These figures can then be used to compare to the WHO guidelines for community noise to get a better perspective on the likelihood of noise nuisance being generated.
- 5.2.2 The rear outdoor seating area of the premises is small and can comfortably hold approximately 30 people at any one time. As there will be no music present in this area there will only be noise from talking. As the area is expected to be more of a quiet escape from the restaurant, the levels are unlikely to exceed those stated in the DEFRA report, and also unlikely to push up into the next category that would constitute as a 'busy crowd'.
- 5.2.3 Assuming the outdoor measured value is constant (68dbA $L_{Aeq,t}$) this can also be put into the distance calculation formula to predict the noise impact at the nearest NSR façade from the outdoor area alone.

$$Lp2 = Lp1 - 20\log\left(\frac{R2}{R1}\right)$$

Where;

L1 = Sound Pressure at Point 1 (68dBA)

L2 = Sound Pressure at Point 2

R1 = Distance from source to Point 1 (1m)

R2 = Distance from source to Point 2 (16m)

$$Lp2 = \underline{\underline{43.9dBA}}$$

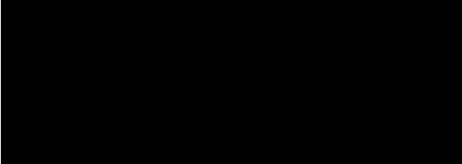
- 5.2.3 If the patron noise is then compared against the WHO guidelines for community noise it can be seen that noise nuisance is unlikely to occur. This based on the external value outside of bedrooms for sleep disturbance with windows open being set at 45dB. This value is 1db above the predicted impact from the patron noise from the bar/restaurant.

6.0 Conclusion and Further Comments

6.1 Discussion of Levels

- 6.1.1 The specific noise level of the noise generated by the cafe/restaurant is below both the BS4142:2014 and IOA guidelines to expect adverse comment during the day period. This is based on the outdoor seating area being at capacity and the door from the main restaurant area being left open (therefore the worst-case scenario).
- 6.1.2 Patron noise has also been considered in this report to look at the noise impact of having customers in the rear outdoor area; either as seated restaurant guests, or during later hours as a social area away from the noise inside the main restaurant. The levels details in the DEFRA pubs and clubs phase I report indicate values of 65-70dB. Either figure would result in levels below those stated in the WHO guidelines for community noise. Therefore, patron noise is also not expected to be classed as a noise nuisance risk if the cafe/restaurant was allowed to use the fully permitted hours up to 9pm externally and 11pm internally.
- 6.1.3 Noise complaints are not always due to the levels of noise that are being created. In some cases the ability to view a person or people making noise increases the likelihood of complaints. This is discussed in the consideration of the context of the perceived noise as part of the BS4142:2014 assessment procedure. Statistically complaints for noise occur more frequently when the noise source can either be identified or viewed.
- 6.1.4 With the above in mind, it is recommended that a 'privacy screen' is erected between the garden areas of the Bobbys cafe/restaurant and the Parade residential area. The values measured mean that the barrier doesn't need to provide any specific noise attenuation but the presence of such a barrier will reduce any patron noise from the garden further still, and provide a visual barrier between the garden and the residents. It can also be used as a method to improve the aesthetics of the garden in the direction of The Parade. This does not have to be a complete barrier, just something that prevents all areas of the outdoor seating area being in direct view of the residents. This suggestion is also made on the basis that there is only a small margin of error (despite the worst-case scenarios being used in this report) and therefore the visual aspect of the perceived noise may result in complaints that are not numerically warranted.

7.0 Credentials

Name	Title	Credentials
James Flitton BSc AMIOA	Acoustic Consultant	Associate Member Institute of Acoustics
		IOA Diploma in Acoustics & Noise Control
		CSCS Professionally Qualified person
		Affiliate Member of IOR
Signed		

Appendix A – Acoustic Terminology











Parameter	Description
Ambient Noise Level	The totally encompassing sound in a given situation at a given time, usually composed sound from many sources both distant and near ($L_{Aeq,T}$).
Decibel (dB)	A scale for comparing the ratios of two quantities, including sound pressure and sound power. The difference in level between two sounds s_1 and s_2 is given by $20 \log_{10}(s_1/s_2)$. The decibel can also be used to measure absolute quantities by specifying a reference value that fixes a point on the scale. For sound pressure, the reference value is $20 \mu\text{Pa}$. The threshold of normal hearing is in the region of 0 dB and 140 dB is the threshold of pain. A change of 1 dB is or perceptible under controlled conditions.
dB(A), L_{Ax}	Decibels measured on a sound level meter incorporating a frequency weighting (A) which differentiates between sounds of different frequency (pitch) in a similar way to the ear. Measurements in dB(A) broadly agree with people's assessment of loudness. A change of 1 dB(A) is the minimum perceptible under normal conditions, and a change of 10 dB(A) corresponds roughly to halving or doubling the loudness of a sound. The background noise in a living room may be about 30 dB(A); normal conversation about 60 dB(A) at 1 metre; heavy road traffic about 80 dB(A) at 10 metres; the level near a pneumatic drill about 100 dB(A)
Fast Time Weighting	Setting on sound level meter, denoted by a subscript F, that determines the speed at which the instrument responds to changes in the amplitude of any measured signal. The fast time weighting can lead to higher values than the slow time weighting when rapidly changing signals are measured. The average time constant for the fast response setting is 0.125 (1/8) second.
Free-field	Sound pressure level measured outside, far away from reflecting surfaces (except the ground), usually taken to mean at least 3.5 metres.
Façade	Sound pressure level measured at a distance of 1 metre in front of a large sound reflecting object such as a building façade.
$L_{Aeq,T}$	A noise level index called the equivalent continuous noise level over the time period T. This level is that of a notional steady sound that would contain the same amount of sound energy as the actual, possibly fluctuating, sound that was recorded.
$L_{max,T}$	A noise level index defined as the maximum noise level recorded during a noise event over the period T. L_{max} is sometimes used for the assessment of occasional loud noises, which may have little effect on the overall L_{eq} noise level but will still affect the noise environment. Unless described otherwise, it is measured using the 'fast' sound level meter response.
$L_{10,T}$	A noise level index. The noise level exceeded for 10% of the time over the period T. L_{10} can be considered to be the "average maximum" noise level. Generally used to describe road noise. $L_{A10,18h}$ is the A-weighted arithmetic average of the 18 hourly $L_{A10,1h}$ values from 06:00-24:00.
$L_{90,T}$	A noise level index. The noise level exceeded for 90% of the time over the period T. Generally used to describe background noise level.

Appendix B – Survey Instrumentation

Type	Manufacturer	Model	Serial Number	Last Cal	Cal Due
SLM	NTi	XL2-TA	A2A-18475-E0	19/10/2022	18/10/2024
Pre-amp	NTi	MA220	9378	19/10/2022	18/10/2024
Microphone	NTi	MC230A	A19093	19/10/2022	18/10/2024
Calibrator	NTi	CAL200	19829	20/11/2023	19/11/2024
SLM	NTi	XL2-TA	A2A-18928-E0	10/05/2023	09/05/2025
Pre-amp	NTi	MA220	9785	10/05/2023	09/05/2025
Microphone	NTi	MC230A	A20919	10/05/2023	09/05/2025

Appendix C – Weather Conditions Chart Used

(Blank Version)

Weather Conditions				
Measurement Location	Date/Time	Description	Beginning of Survey	End of Survey
		Temperature:		
<p style="text-align: center;">Cloud Cover</p> <p>Symbol Scale in oktas (eighths)</p> <p> 0 Sky completely clear</p> <p> 1</p> <p> 2</p> <p> 3</p> <p> 4 Sky half cloudy</p> <p> 5</p> <p> 6</p> <p> 7</p> <p> 8 Sky completely cloudy</p> <p> (9) Sky obstructed from view</p>		Precipitation:		
		Cloud cover (oktas - see guide)		
		Presence of fog/snow/ice		
		Presence of damp roads/wet ground		
		Wind Speed (m/s)		
		Wind Direction		
		Conditions that may cause temperature inversion (i.e. calm nights with no cloud)		

Appendix D – CadnaA Calculations

Receiver
 Name: NSR1
 ID:
 X: 30516852.67 m
 Y: 5839875.16 m
 Z: 10.10 m

vert. Area Source, ISO 9613, Name: "", ID: ""

Nr.	X (m)	Y (m)	Z (m)	Refl.	DEN	Freq. (Hz)	Lw dB(A)	lva dB	Optime dB	K0 (dB)	Di (dB)	Adiv (dB)	Aatm (dB)	Agr (dB)	Afol (dB)	Ahous (dB)	Abar (dB)	Cmet (dB)	RL (dB)	Lr dB(A)
1	30516852.69	5839874.19	1.67	0	DEN	500	39.0	2.8	0.0	3.0	0.0	29.6	0.0	0.1	0.0	0.0	0.0	0.0	0.0	15.1
2	30516852.65	5839876.18	1.67	0	DEN	500	39.0	3.1	0.0	3.0	0.0	29.6	0.0	0.1	0.0	0.0	0.0	0.0	0.0	15.4
3	30516852.69	5839874.19	0.67	0	DEN	500	39.0	2.8	0.0	3.0	0.0	30.5	0.0	0.2	0.0	0.0	0.0	0.0	0.0	14.0
4	30516852.65	5839876.18	0.67	0	DEN	500	39.0	3.1	0.0	3.0	0.0	30.5	0.0	0.2	0.0	0.0	0.0	0.0	0.0	14.3
5	30516852.69	5839874.19	2.67	0	DEN	500	39.0	2.8	0.0	3.0	0.0	28.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	16.3
6	30516852.65	5839876.18	2.67	0	DEN	500	39.0	3.1	0.0	3.0	0.0	28.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	16.6

Area Source, ISO 9613, Name: "", ID: ""

Nr.	X (m)	Y (m)	Z (m)	Refl.	DEN	Freq. (Hz)	Lw dB(A)	lva dB	Optime dB	K0 (dB)	Di (dB)	Adiv (dB)	Aatm (dB)	Agr (dB)	Afol (dB)	Ahous (dB)	Abar (dB)	Cmet (dB)	RL (dB)	Lr dB(A)
7	30516857.79	5839872.42	0.00	0	DEN	500	60.3	7.4	0.0	0.0	0.0	32.3	0.0	1.5	0.0	0.0	0.0	0.0	0.0	33.9
9	30516859.89	5839872.42	0.00	0	DEN	500	60.3	7.4	0.0	0.0	0.0	33.1	0.0	2.0	0.0	0.0	0.0	0.0	0.0	32.6
11	30516856.74	5839873.59	0.00	0	DEN	500	60.3	7.4	0.0	0.0	0.0	31.8	0.0	1.2	0.0	0.0	0.0	0.0	0.0	34.7
13	30516856.74	5839875.95	0.00	0	DEN	500	60.3	7.4	0.0	0.0	0.0	31.8	0.0	1.1	0.0	0.0	0.0	0.0	0.0	34.9
15	30516859.89	5839877.13	0.00	0	DEN	500	60.3	7.4	0.0	0.0	0.0	33.0	0.0	1.9	0.0	0.0	0.0	0.0	0.0	32.8
19	30516857.79	5839877.13	0.00	0	DEN	500	60.3	7.4	0.0	0.0	0.0	32.2	0.0	1.5	0.0	0.0	0.0	0.0	0.0	34.1
22	30516860.94	5839875.95	0.00	0	DEN	500	60.3	7.4	0.0	0.0	0.0	33.3	0.0	2.1	0.0	0.0	0.0	0.0	0.0	32.3
25	30516860.94	5839873.59	0.00	0	DEN	500	60.3	7.4	0.0	0.0	0.0	33.4	0.0	2.2	0.0	0.0	0.0	0.0	0.0	32.2

Receiver
 Name: NSR2
 ID:
 X: 30516855.24 m
 Y: 5839867.68 m
 Z: 10.10 m

Area Source, ISO 9613, Name: "", ID: ""

Nr.	X (m)	Y (m)	Z (m)	Refl.	DEN	Freq. (Hz)	Lw dB(A)	lva dB	Optime dB	K0 (dB)	Di (dB)	Adiv (dB)	Aatm (dB)	Agr (dB)	Afol (dB)	Ahous (dB)	Abar (dB)	Cmet (dB)	RL (dB)	Lr dB(A)
8	30516857.01	5839873.30	0.00	0	DEN	500	60.3	6.9	0.0	0.0	0.0	32.4	0.0	1.6	0.0	0.0	0.0	0.0	0.0	33.2
10	30516857.27	5839875.36	0.00	0	DEN	500	60.3	6.9	0.0	0.0	0.0	33.2	0.0	2.1	0.0	0.0	0.0	0.0	0.0	31.9
12	30516857.92	5839872.27	0.00	0	DEN	500	60.3	6.9	0.0	0.0	0.0	32.1	0.0	1.4	0.0	0.0	0.0	0.0	0.0	33.6
14	30516860.02	5839872.27	0.00	0	DEN	500	60.3	6.9	0.0	0.0	0.0	32.6	0.0	1.7	0.0	0.0	0.0	0.0	0.0	32.8
16	30516855.96	5839877.93	0.00	0	DEN	500	60.3	-10.5	0.0	0.0	0.0	34.2	0.0	2.6	0.0	0.0	0.0	0.0	0.0	13.0
18	30516856.09	5839875.47	0.00	0	DEN	500	60.3	-1.7	0.0	0.0	0.0	33.1	0.0	2.0	0.0	0.0	0.0	0.0	0.0	23.4
21	30516855.83	5839873.41	0.00	0	DEN	500	60.3	-1.7	0.0	0.0	0.0	32.3	0.0	1.5	0.0	0.0	0.0	0.0	0.0	24.7
24	30516855.96	5839876.72	0.00	0	DEN	500	60.3	1.3	0.0	0.0	0.0	33.7	0.0	2.3	0.0	0.0	0.0	0.0	0.0	25.6
27	30516855.70	5839878.22	0.00	0	DEN	500	60.3	-29.6	0.0	0.0	0.0	34.3	0.0	2.7	0.0	0.0	0.0	0.0	0.0	-6.3
29	30516859.02	5839876.93	0.00	0	DEN	500	60.3	11.1	0.0	0.0	0.0	34.0	0.0	2.5	0.0	0.0	0.0	0.0	0.0	34.8
31	30516861.12	5839875.75	0.00	0	DEN	500	60.3	6.7	0.0	0.0	0.0	34.0	0.0	2.5	0.0	0.0	0.0	0.0	0.0	30.4
34	30516861.12	5839873.40	0.00	0	DEN	500	60.3	6.7	0.0	0.0	0.0	33.3	0.0	2.1	0.0	0.0	0.0	0.0	0.0	31.5

vert. Area Source, ISO 9613, Name: "", ID: ""

Nr.	X (m)	Y (m)	Z (m)	Refl.	DEN	Freq. (Hz)	Lw dB(A)	lva dB	Optime dB	K0 (dB)	Di (dB)	Adiv (dB)	Aatm (dB)	Agr (dB)	Afol (dB)	Ahous (dB)	Abar (dB)	Cmet (dB)	RL (dB)	Lr dB(A)
36	30516852.69	5839873.74	0.67	0	DEN	500	39.0	0.1	0.0	3.0	0.0	32.2	0.0	1.4	0.0	0.0	7.6	0.0	0.0	0.8
39	30516852.67	5839875.20	0.67	0	DEN	500	39.0	2.8	0.0	3.0	0.0	32.8	0.0	1.7	0.0	0.0	6.9	0.0	0.0	3.4
42	30516852.65	5839876.69	0.67	0	DEN	500	39.0	0.2	0.0	3.0	0.0	33.5	0.0	1.9	0.0	0.0	6.4	0.0	0.0	0.3
45	30516852.69	5839873.74	1.67	0	DEN	500	39.0	0.1	0.0	3.0	0.0	31.6	0.0	0.5	0.0	0.0	7.7	0.0	0.0	2.2
48	30516852.67	5839875.20	1.67	0	DEN	500	39.0	2.8	0.0	3.0	0.0	32.3	0.0	0.6	0.0	0.0	7.0	0.0	0.0	4.9
50	30516852.65	5839876.69	1.67	0	DEN	500	39.0	0.2	0.0	3.0	0.0	33.0	0.0	0.7	0.0	0.0	6.5	0.0	0.0	2.0
52	30516852.69	5839873.74	2.67	0	DEN	500	39.0	0.1	0.0	3.0	0.0	30.9	0.0	0.1	0.0	0.0	7.9	0.0	0.0	3.1
54	30516852.67	5839875.20	2.67	0	DEN	500	39.0	2.8	0.0	3.0	0.0	31.7	0.0	0.1	0.0	0.0	7.1	0.0	0.0	5.8
56	30516852.65	5839876.69	2.67	0	DEN	500	39.0	0.2	0.0	3.0	0.0	32.6	0.0	0.1	0.0	0.0	6.6	0.0	0.0	2.9

Receiver
 Name: NSR3
 ID:
 X: 30516852.85 m
 Y: 5839859.89 m
 Z: 9.98 m

Area Source, ISO 9613, Name: "", ID: ""

Nr.	X (m)	Y (m)	Z (m)	Refl.	DEN	Freq. (Hz)	Lw dB(A)	I/a dB	Optime dB	K0 (dB)	Di (dB)	Adiv (dB)	Aatm (dB)	Agr (dB)	Afol (dB)	Ahous (dB)	Abar (dB)	Cmet (dB)	RL (dB)	Lr dB(A)
33	30516859.35	5839872.45	0.00	0	DEN	500	60.3	9.3	0.0	0.0	0.0	35.8	0.0	3.4	0.0	0.0	0.0	0.0	0.0	30.4
35	30516857.20	5839873.68	0.00	0	DEN	500	60.3	9.5	0.0	0.0	0.0	35.9	0.0	3.5	0.0	0.0	5.5	0.0	0.0	24.8
38	30516856.40	5839874.30	0.00	0	DEN	500	60.3	-1.5	0.0	0.0	0.0	36.0	0.0	3.6	0.0	0.0	7.2	0.0	0.0	11.9
41	30516856.12	5839875.62	0.00	0	DEN	500	60.3	6.2	0.0	0.0	0.0	36.5	0.0	3.8	0.0	0.0	8.1	0.0	0.0	18.0
43	30516856.65	5839877.83	0.00	0	DEN	500	60.3	0.6	0.0	0.0	0.0	37.4	0.0	4.3	0.0	0.0	7.9	0.0	0.0	11.2
46	30516858.45	5839877.04	0.00	0	DEN	500	60.3	8.0	0.0	0.0	0.0	37.3	0.0	4.2	0.0	0.0	5.2	0.0	0.0	21.6
47	30516860.21	5839876.38	0.00	0	DEN	500	60.3	8.3	0.0	0.0	0.0	37.3	0.0	4.2	0.0	0.0	0.0	0.0	0.0	27.0
49	30516861.24	5839874.44	0.00	0	DEN	500	60.3	9.0	0.0	0.0	0.0	36.8	0.0	4.0	0.0	0.0	0.0	0.0	0.0	28.5

vert. Area Source, ISO 9613, Name: "", ID: ""

Nr.	X (m)	Y (m)	Z (m)	Refl.	DEN	Freq. (Hz)	Lw dB(A)	I/a dB	Optime dB	K0 (dB)	Di (dB)	Adiv (dB)	Aatm (dB)	Agr (dB)	Afol (dB)	Ahous (dB)	Abar (dB)	Cmet (dB)	RL (dB)	Lr dB(A)
51	30516852.67	5839875.22	0.67	0	DEN	500	39.0	6.0	0.0	3.0	0.0	36.1	0.0	3.0	0.0	0.0	15.4	0.0	0.0	-6.6
53	30516852.67	5839875.22	1.67	0	DEN	500	39.0	6.0	0.0	3.0	0.0	35.8	0.0	1.0	0.0	0.0	15.8	0.0	0.0	-4.8
55	30516852.67	5839875.22	2.67	0	DEN	500	39.0	6.0	0.0	3.0	0.0	35.6	0.0	0.1	0.0	0.0	16.0	0.0	0.0	-3.8

Receiver
 Name: NSR4
 ID:
 X: 30516857.11 m
 Y: 5839852.54 m
 Z: 10.07 m

Area Source, ISO 9613, Name: "", ID: ""

Nr.	X (m)	Y (m)	Z (m)	Refl.	DEN	Freq. (Hz)	Lw dB(A)	I/a dB	Optime dB	K0 (dB)	Di (dB)	Adiv (dB)	Aatm (dB)	Agr (dB)	Afol (dB)	Ahous (dB)	Abar (dB)	Cmet (dB)	RL (dB)	Lr dB(A)
17	30516855.82	5839873.59	0.00	0	DEN	500	60.3	1.4	0.0	0.0	0.0	38.4	0.0	4.8	0.0	0.0	0.0	0.0	0.0	18.4
20	30516856.21	5839874.72	0.00	0	DEN	500	60.3	6.3	0.0	0.0	0.0	38.7	0.0	5.0	0.0	0.0	0.0	0.0	0.0	22.8
23	30516858.36	5839873.30	0.00	0	DEN	500	60.3	12.2	0.0	0.0	0.0	38.3	0.0	4.8	0.0	0.0	0.0	0.0	0.0	29.4
26	30516855.91	5839878.18	0.00	0	DEN	500	60.3	-12.6	0.0	0.0	0.0	39.8	0.1	5.6	0.0	0.0	0.0	0.0	0.0	2.3
28	30516856.27	5839877.98	0.00	0	DEN	500	60.3	-5.7	0.0	0.0	0.0	39.7	0.1	5.6	0.0	0.0	0.0	0.0	0.0	9.3
30	30516859.58	5839876.33	0.00	0	DEN	500	60.3	12.6	0.0	0.0	0.0	39.3	0.1	5.3	0.0	0.0	0.0	0.0	0.0	28.2
32	30516861.62	5839874.01	0.00	0	DEN	500	60.3	5.9	0.0	0.0	0.0	38.7	0.0	5.0	0.0	0.0	0.0	0.0	0.0	22.5

vert. Area Source, ISO 9613, Name: "", ID: ""

Nr.	X (m)	Y (m)	Z (m)	Refl.	DEN	Freq. (Hz)	Lw dB(A)	I/a dB	Optime dB	K0 (dB)	Di (dB)	Adiv (dB)	Aatm (dB)	Agr (dB)	Afol (dB)	Ahous (dB)	Abar (dB)	Cmet (dB)	RL (dB)	Lr dB(A)
37	30516852.67	5839875.22	0.67	0	DEN	500	39.0	6.0	0.0	3.0	0.0	38.9	0.0	4.2	0.0	0.0	9.1	0.0	0.0	-4.3
40	30516852.67	5839875.22	1.67	0	DEN	500	39.0	6.0	0.0	3.0	0.0	38.8	0.0	1.4	0.0	0.0	9.2	0.0	0.0	-1.6
44	30516852.67	5839875.22	2.67	0	DEN	500	39.0	6.0	0.0	3.0	0.0	38.7	0.0	0.2	0.0	0.0	9.3	0.0	0.0	-0.3